SUSTAINABLE RESOURCE
DEVELOPMENT

## ALBERTA SCALING MANUAL

## APPENDICES

### 11.0 Appendices

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Appendix 1 - Application for Scale Site
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## Appendix 2 - Mass Scaling for the Smaller Timber Operation

## Application

There are many smaller timber operations in Alberta who do not have the assurance of a defined long-term wood supply, and an on-site weigh scale for timber harvest accounting is not an economic reality.

Weigh scale accounting of harvested timber is a proven and effective method authorized by the Public Land and Forest Division (PLFD). To make this system possible for smaller timber operations, the use of departmental approved weigh scales owned by another person/company will be considered. These approvals are deviations from standard accepted practices and are therefore limited to the following:

Operations which currently determine the harvested volumes on a manufacture basis and which are:

1. Processing community timber and/or directed FMA incidental (and which may include private or salvage) timber.
2. Approved by the local PLFD area office for this purpose. (Refer to "Agreement").

To obtain consideration for mass scaling the first step is to complete a "Mass Scaling Agreement". (Refer to sample form). This form is to be fully completed by all parties and a copy forwarded to the Provincial Scaling Supervisor.

Before a PLFD representative signs the form that person will address inventories, fixed tare weight determinations, and ensure all mass scaling practices and are in place with the timber operator. (Refer to those sections following the sample form).

## Mass Scaling Agreement

I, $\qquad$ of $\qquad$ ,
have read, and understand, the requirements of weigh scale accounting for timber (attached). I hereby request that all timber, or as otherwise directed by the Public Land and Forest Division (PLFD), which is delivered to my mill (processing site) located at
$\qquad$ , be accounted for by weighing across the weigh
scales of $\qquad$ . Sample log scaling or the application if fixed weight to volume ratios will be implemented as directed by the PLFD. The request date for commencing weigh scale accounting is $\qquad$ . I am in agreement to follow proper procedures for weigh scale accounting and that I shall maintain and submit weigh scale records to the PLFD as required. I further understand that I am to abide by all relevant legislation in the Forests Act and its associated regulations, and that failure to do so may result in penalty action and/or forfeiture of this agreement.

## Applicant

Signed: $\qquad$ Signed:

## Weigh Scale Owner

Printed Name: $\qquad$

Date: $\qquad$

Public Land and Forest Division Representative

Printed Name: $\qquad$

Phone Number: $\qquad$
Date:

Signature $\qquad$

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## Handling Existing Inventory

Manufactured products and log inventory hauled into a yard prior to approving the use of the weigh scale is to be segregated from weigh scaled timber. Timber manufactured and sold under the non-scale system is reported separately.

## Scale Populations

Scaling populations and sample intensities are to be established through discussions with the Forest Area and Company. Form TM262 "Scaling Populations", is to be completed each timber year.

## Weighing

1. Weights and date/times are to be printed on every load ticket (using a printer attached to the weigh scale).
2. Gross weights are to be taken for every load.
3. Tare weights will be required for every sample load and are to be taken immediately after unloading.
4. Average tare weights will be accepted providing the procedures for establishing and testing fixed tare weights is followed (Refer to the section below titled "Procedure for Average Tare Weights").

## Sample Load Selection and Scaling

- Where sample loads are requested, sample cards or random load generators will be used to select the scale loads as they cross the scale.
- Sample scale trees are to be bucked and the scaling is to be done by a permitted scaler.
- The scale loads are to be left in the same condition as they were scaled until checked scaled or released by the local PLFD area staff.


## Weigh Scale Records

- A mill number and mill code will be assigned by the Forest Management Branch of the PLFD, and which are to be used on all records requiring such.
- The weigh scale information must be summarized on departmental approved forms and submitted within 21 days following each month of weigh scale activity.
- Forms which must be completed and submitted include the TM35 "Weigh Scale Load Record Sheet" and TM44 "Volume Compilation Sheet". The sample scale loads are to be compiled using the Micro Logscale program and submitted on a computer disk along with the other required scale forms.
- Unless authorized by PLFD area staff, all timber including private and salvage timber hauled to the mill site is to be accounted for by the weigh scale process.

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## Procedure for Average Tare Weights

Weigh scaling for the smaller timber operator provides for the use of average tare weights. This acceptance of this practice will be subject to the following requirements:

1. The average tare must be based on at least 10 sample weights for each truck. If a truck changes configuration the average must be re-established by the same process.
2. The average tare weight for any one truck must not have a coefficient of variation of more than $\pm 2 \%$. Trucks having a variance of more than $\pm 2 \%$ must continue to reweigh out until the variance is within range.
3. The average tare must be randomly sampled at a minimum of 20 load intervals to determine if the weight is still within $\pm 2 \%$ of the average. If not, repeat step 1 .
4. Calculation of the average tare and the variance must be documented and included with scale data submissions.

The average tare cannot be used for sample loads. The trucks must obtain tare weights for sample loads.

| Truck | Tare Weight (kg) | Difference from Average | Difference <br> Squared |
| :---: | :---: | :---: | :---: |
| 1 | 15350 | 4 | 16 |
|  | 15240 | 114 | 12996 |
|  | 15360 | -6 | 36 |
|  | 15310 | 44 | 1936 |
|  | 15390 | -36 | 1296 |
|  | 15260 | 94 | 8836 |
|  | 15160 | 194 | 37636 |
|  | 15490 | -136 | 18496 |
|  | 15350 | 4 | 16 |
|  | 15630 | -276 | 76176 |
|  | $\overline{153540}$ |  | $\overline{157440}$ |

$$
\begin{aligned}
& \text { Average tare }=\frac{153540}{10}=15354 \\
& \mathrm{SD}=\sqrt{ } \frac{157440}{(10-1)}= \pm 132 \text { C.V. } \% \\
&=\frac{\text { SD }}{\text { Avg. Tare }} \times 100 \%=0.86 \%
\end{aligned}
$$

## Appendix 3 - Example of Mass Scale Analysis

| Load <br> No. | Net <br> Weight | Sw \& Pl <br> Scale | Fb <br> Scale | Total <br> Scale | Scale <br> Estimate | Diff. | Diff. ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 38 | 43400 | 42.196 | 0.000 | 42.196 | 51.764 | +9.568 | 91.547 |
| 81 | 36360 | 41.682 | 0.000 | 41.682 | 43.367 | +1.685 | 2.839 |
| 174 | 48220 | 60.829 | 0.000 | 60.839 | 57.513 | -3.326 | 11.062 |
| 19 | 43400 | 56.057 | 1.161 | 57.218 | 51.764 | +5.454 | 29.746 |
| 38 | 37780 | 49.188 | 1.708 | 50.896 | 45.061 | -5.835 | 34.047 |
| 141 | 50220 | 55.902 | 0.000 | 55.902 | 59.898 | +3.996 | 15.968 |
| 153 | 44980 | 50.001 | 0.487 | 50.488 | 53.648 | +3.160 | 9.986 |
| 256 | 38460 | 44.845 | 0.123 | 44.968 | 45.872 | +0.904 | 0.817 |
| 277 | 44760 | 53.628 | 1.021 | 54.649 | 53.386 | -1.263 | 1.595 |
| 177 | $\underline{41960}$ | 49.816 | 3.666 | $\underline{53.482}$ | $\underline{50.046}$ | -3.436 | $\underline{11.806}$ |

$$
\begin{array}{cc}
\text { Ratio }=\frac{429540}{512.320}=838.421 & \text { Avg. Volume/Load }=\frac{512.320}{10}=51.232 \\
\mathrm{SD}=\sqrt{\frac{209.413}{(10-1)}}=4.823 & \mathrm{CV} \%=\frac{4.823 \times 100}{51.232}=9.41 \%
\end{array}
$$

Projected Cut: $\quad 5,000,000 \mathrm{fbm}\left(21500 \mathrm{~m}^{3}\right)$

$$
\begin{array}{ll} 
& \mathrm{N}=\frac{21.500}{51.232}=420 \text { loads } \\
& \mathrm{n}=\frac{N t^{2} C^{2}}{N E^{2}+t^{2} C^{2}} \\
\text { Where: } \quad & \mathrm{n}=\text { number of samples } \\
& \mathrm{N}=\text { number of loads } \\
& \mathrm{t}=\text { probability }(2) \\
& \mathrm{E}=\text { allowable sampling error }
\end{array}
$$

1st Calculation $\quad \mathrm{n}=\frac{420(2)^{2} x(9.41)^{2}}{420(5)^{2}+\left[(2)^{2} x(9.41)^{2}\right]}=\frac{148761}{10854}=13.7(14$ samples $)$
Revised $\mathrm{t}=(14-1=13)=2.16$
2nd Calculation $\quad \mathrm{n}=\frac{420(2.16)^{2} x(9.41)^{2}}{420(5)^{2}+\left[(2.16)^{2} x(9.41)^{2}\right]}=\frac{173515}{10913}=15.8(16$ samples $)$

$$
\% \text { Sampling }=\frac{15.8}{420} x 100=3.7=4 \%
$$

## Appendix 4 - Tree Length Scaling

Example of Calculation of Sampling Intensity for Butt Distribution

| Sample <br> Number | Stems | Sample <br> Volume <br> $\mathbf{m}^{\mathbf{3}(1000 x)}$ | Average <br> Vol./Stem <br> $\mathbf{m}^{\mathbf{3}(1000 x)}$ | Difference <br> from <br> Group <br> Estimate | Difference <br> Squared |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 24 | 14753 | 615 | -216 | 46656 |
| 2 | 20 | 25536 | 1277 | 446 | 198916 |
| 3 | 27 | 26427 | 979 | 148 | 21904 |
| 4 | 11 | 9490 | 863 | 32 | 1024 |
| 5 | 29 | 26427 | 911 | 80 | 6400 |
| 6 | 19 | 12064 | 635 | -196 | 38416 |
| 7 | 9 | 7975 | 886 | 55 | 3025 |
| 8 | 23 | 19731 | 858 | 27 | 729 |
| 9 | 19 | 13151 | 692 | -139 | 19321 |
| 10 | 23 | 14013 | 609 | -222 | 49284 |
|  | 204 | 169567 | 831 |  | 385675 |

Total stems tallied $=4000$
Avg. trees/sample 204/10=20.4
$\sum D^{2}=385675$
$\mathrm{SD}=\sqrt{\frac{385675}{(10-1)}}=207 \quad$ Avg. volume $/$ stem $=\frac{169567}{204}=831$
C.V. $\%=\frac{207 \times 100}{831}=24.9 \%$
$\mathrm{n}=\frac{\mathrm{Nt}^{2} \mathrm{C}^{2}}{\mathrm{NA}^{2}+\mathrm{t}^{2} \mathrm{C}^{2}}$
Where: $\mathrm{N}=4000 / 20.4=196$
$\mathrm{t}=2$
$\mathrm{A}=5$
$C=24.9$
$\mathrm{n}=\frac{196(2)^{2}(24.9)^{2}}{196(5)^{2}+(2)^{2}(24.9)^{2}}=66$ samples
$196(5)^{2}+(2)^{2}(24.9)^{2}$
$\%$ sampling $=\underline{66 \times 100}=33.7 \%$

# Appendix 5 - Common Stains and Defects Found When Scaling 

## STAINS

## 1. Red Heart Stain - Pine and Spruce

This is an early stage of Phellinus pini (Thore:Fr.) Ames, referred to as white pitted rot or white pocket rot. This rot generally attacks pine and spruce, but does not advance after the tree is cut. The stained wood is as strong as unstained wood and can be used for building construction except where extra strength or unstained appearance is required. Various stages of the rot are referred to as white speck and honeycomb. Firm white speck is still acceptable in the middle grades of lumber.
2. Red Brown Stain - Balsam Fir

This is an early stage of Haematostereum sanguinolentum (Alb. and Sch.:Fr.) Fir., referred to as red heart rot. The rot first shows as a firm red-brown stain, often in streaks. The decay does not advance after the tree has been cut, and the stained wood is not significantly weaker than unstained material. Also, the pulp strength is not likely to be affected by the stain.

## 3. Red stain - Aspen

This stain is a result of Peniophora polygonia (Pers.:Fries) Bourd. \& Galzin, resulting in stained columns coming from infected branches in aspen. The stained wood is suitable for pulp and oriented strandboard with some considerations. There can be some rot pockets or ring separation from an associated rot, which will result in extra fines in the oriented strand- board wafers or in pulp chips. As well, if the material is used for CTMP pulp, bleaching out the stain may be a problem.

## 4. Blue stain - All species

Blue stain often develops in stored logs or on dead trees. This stain often results from mountain pine beetle attacks. It has the most effect on CTMP pulping processes because of the added bleaching cost. Since the stain develops mainly after logging and during storage of the wood, damage can be controlled or prevented to some extent. For kraft pulp processes, oriented strandboard and lumber products, the stain does not present any strength problems.
5. Black stain - Black Poplar

This stain is seen as greyish-black with some brownish pockets and is common in black poplar. Although black stain eliminates the use of black poplar for the CTMP pulping process, it can be bleached out in the kraft pulp processes.

## HEART OR STEM ROTS

1. White Pitted Rot or White Pocket Rot (Phellinus pini [Thore:Fr.] Ames)

This rot generally attacks pine and spruce. The first stage is referred to as red stain. The stained area is as strong as unstained wood. The rot does not advance after the tree is cut. Various stages of the rot are referred to as white speck and honeycomb. Firm white speck is still acceptable in the middle grades of lumber. Wood with advanced rot (honeycomb) is usually quite weak, although it is used for the bottom grades of lumber providing it holds together. It is appropriate to make deductions for honeycomb.
2. Red Heart Rot (Haematostereum sanguinolentum [Alb. \& Sch.:Fr.] Fir.)

This rot is usually associated with balsam fir. The rot first shows as a firm red-brown stain, often in streaks. As it advances, a white rot develops that is light to red-brown in colour, and dry and somewhat stringy. In logs, it usually forms a circular mass around the pith. The most serious problem with the rot is that it causes separation in the annual rings, thus degrading the lumber. In making deductions, look for the white rot developing along the annual rings.
3. White Heart Rot (Phellinus tremulae [Bond.] Bond. \& Boriss., Phellinus igniarius [Linnaeus:Fries] Quel., Fomes igniarius [Linnaeus:Fries] J.Kickx fil.)

This is the most common trunk rot that attacks aspen in Alberta. A prominent black line surrounds and often occurs within the decayed areas. The rot is a yellowish to white colour and has a soft and spongy texture. This rot is very weak and usually crumbles when put through chippers or wafer machines.

## BUTT OR ROOT ROTS

## 1. Armillaria Butt Rot (mostly Armillaria ostoyae [Romagn.] Herink)

Can attack either coniferous or deciduous trees. The yellow, stringy rot is often covered by dark brown fungal material mixed with wood. The decay occurs at the bottom of the tree and tapers off quickly, seldom extending more than 1 m up the tree.

## 2. Brown Cubical Rot (Coniophora puteana [Schum.:Fries] Karst.)

Frequently found as a butt rot in pine and spruce. The decay usually tapers off quickly. This rot is usually referred to in lumber grading as soft rot and is normally trimmed off to make better grades. Deductions for small isolated pockets can be made by making a visual deduction of 1 to 10 cubes.

## Appendix 6 -Definitions

Accuracy - means the degree of agreement with an accepted reference value of individual measurements, test, or observations made under prescribed conditions, or of estimates computed from them, and refers to the success of estimating the true value of quantity

Bark - means all the tissues, including the cambium, taken collectively and forming the exterior covering of the xylem of a tree.

Bias - means consistent or systematic error that will be of the same amount in all individuals of a set of measurements made under similar circumstances; alternatively, a systematic distortion due to some flaw in measurement, to the method of selecting the sample, or to the technique of estimating the parameter.

Bolt - means any short log specifically cut to length
Butt end - the end of larger diameter usually the stump end.
Butt swell - means that part of a log outside its normal taper and extending from where the normal taper ends and the flare begins to the large end of the log.

Catface - means a defect on the surface of a tree or log resulting from a wound where healing has not re-established the normal cross section.

Check - means a lengthwise separation of the wood in a log or piece of timber, which usually extends across the rings of annual growth, commonly resulting from stresses set up in the wood during seasoning.

Coefficient of variation - means an expression of variability among units in the form of the ratio of the standard deviation(s) to the mean ( x ) and is usually expressed by the formula $\mathrm{C}=\mathrm{s} / \mathrm{x}$

Crook - means an abrupt bend or curvature in the length of a log.
Decay - the decomposition of wood substance caused by the action of wood-destroying fungi, resulting in softening, loss of strength and mass, and often change of texture and colur.

Advanced decay - the late stage of decay in which the decompostion is readily recognized, as the wood becomes punky, soft, stringy, pitted or crumbly. Heart rot - means any rot characteristically confined to the heartwood. It generally originates in the living tree.

Butt rot - means any decay or rot developing in, and sometimes characteristically confined to, the base or lower stem of a tree

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Heart rot - any rot generally confined to the heartwood.
Pocket rot - any rot localized in small areas, generally forming rounded or lenshaped cavities, honeycomb decay.

Ring rot - any rot localized mainly in the earlywood of the annual rings, giving a concentric pattern of decayed wood in cross section.

Sap rot - means any rot characteristically confined to the sapwood.
Defect - means any of the following imperfections occurring in and affecting the utility of logs: advanced decay, charred wood, and missing wood.

Fork - means a division of a $\log$ or a stem of a tree into two or more branches
Fuelwood - means roundwood, whole or split, produced for burning.
Hardwoods - trees of the botanical group that generally have broad leaves, in contrast to the conifers. The term has no reference to the actual hardness of the wood.

Heart shake - means a shake that originates at the pith of a $\log$ and extends across the annual rings.

Heartwood - means the inner core of a woody stem wholly composed of nonliving cells and usually differentiated from the outer enveloping layer (sapwood) by its darker colour. It is usually more decay resistant than sapwood.

Local volume table - means a table showing, for one or more species, the average cubic contents for tree lengths by diameter classes, within a smaller geographic region.

Mass - means the property of a body that is a measure of its inertia that is commonly taken as a measure of the amount of material it contains, and that causes it to have weight in a gravitational field.

Moisture content - means the mass of water in wood expressed as a percentage of its total mass.
Net Volume - means the volume remaining after all deductions for defect from gross volume have been made; in stacked measure, deductions include voids.

Ovendry - means a condition in which the wood has ceased to lose moisture after being subjected to a temperature of $103+/-2^{\circ} \mathrm{C}$ in a ventilated oven, for purposes of determining moisture content.

Piece - means a part of a whole (as of a tree)

Pile face - means, in tree-length scaling, the surface formed by butt ends that have been piled with the butts all aligned in a nearly vertical plane.

Precision - means the closeness of agreement among a set of measurements made under prescribed conditions, and refers to the clustering of sample values about their own average.

Roundwood - means any section of the stem, or of the thicker branches, of a tree of commercial value that has been felled or cut but has not been processed beyond removing the limbs or bark, or both, or splitting the section (for fuelwood).

Sample size - means the number of items, specimens, observations, or measurements to be included in the sample.

Sampling Error - the difference between a true value for a population and an estimate of this value, which is due to the fact that only sample values are being observed. The standard error is a measure of the sampling error.

Sapwood - means the living wood of pale colour near the outside of the log. Under most conditions the sapwood is more susceptible to decay than heartwood.

Scale - means the measured or estimated quantity, expressed as the volume, or area, or length, or mass, or number of products obtained from trees after they are felled.

Scaler - means a person qualified to scale primary forest products and usually licensed or appointed by a government agency.

Shake - means a separation along the grain of a log or tree and occurring between or across the annual rings but not extending from one surface to another.

Ring shake - means a shake that partially or completely encircles the pith.
Softwood - means, generally, one of the botanical groups of trees that in most cases have needle or scale like leaves; the conifers. The term has no reference to the actual hardness of the wood.

Stack - means, for scaling purpose, an orderly arrangement of bolts less than or equal to the 2.60 m class in length.

Stacked cubic metre - means the total amount of wood, bark, and airspace contained in a stack of roundwood, as determined by its external dimensions, equal to $1 \mathrm{~m}^{3}$.

Standard deviation - means the square root of the variance, and is symbolized by s.

Standard error of the mean - a measure of the variability of the sample means.
Sweep - means a gradual curve in the length of a log, as distinct from an abrupt bend or curvature.

Taper - means the progressive decrease or increase in the diameter of a log from one end or point on its length to another.

Tolerance - means the total range of variation permitted for a required size.
Tree length - the bole of a tree that has been felled, had the top removed, and generally but not necessarily been limbed.

Variance (of a population) - means a measure of the dispersion of individual unit values about their mean.

Wood - means the hard fibrous substance, basically xylem, that makes up the greater part of the stems and branches of trees or shrubs, beneath the bark.

Woodchip - a small, thin, flat piece of wood cut from a larger piece of wood by knife action, mechanically operated. A woodchip shall show two knife cuts and its width shall always be greater than its thickness.

## Appendix 7

## SCALING TABLES

1. Basal Area

Basal Area
2. Volume of Cylinders Volume of Cylinders
3. t Adjustment Table t Adjustment Table
4. Samples Required Samples Required
5. Percent Samples Required Percent Samples Required
6. Summary of General Conversion Factors Conversion Factors
7. Smalian Half Volume Table Smalian $1 / 2$ Volume Table

| Table 1 - Basal Area -m² (1000x) |  |  |  |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Diameter }(\mathrm{cm}) \\ 4 \end{gathered}$ | Basal Area 1 | Diameter (cm) $42$ | Basal Area $139$ |
| 6 | 3 | 44 | 152 |
| 8 | 5 | 46 | 166 |
| 10 | 8 | 48 | 181 |
| 12 | 11 | 50 | 196 |
| 14 | 15 | 52 | 212 |
| 16 | 20 | 54 | 229 |
| 18 | 25 | 56 | 246 |
| 20 | 31 | 58 | 264 |
| 22 | 38 | 60 | 283 |
| 24 | 45 | 62 | 302 |
| 26 | 53 | 64 | 322 |
| 28 | 62 | 66 | 342 |
| 30 | 71 | 68 | 363 |
| 32 | 80 | 70 | 385 |
| 34 | 91 | 72 | 407 |
| 36 | 102 | 74 | 430 |
| 38 | 113 | 76 | 454 |
| 40 | 126 | 78 | 478 |

Table 2 - Volume of Cylinders - m ${ }^{3}$ (1000x)

| $\begin{gathered} \hline \text { Diameter } \\ (\mathrm{cm}) \end{gathered}$ | $\begin{gathered} \hline \text { Length } \\ 2.4 \mathrm{~m} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Length } \\ 2.6 \mathrm{~m} \end{gathered}$ | Diameter (cm) | $\begin{gathered} \text { Length } \\ 2.4 \mathrm{~m} \end{gathered}$ | $\begin{gathered} \hline \text { Length } \\ 2.6 \mathrm{~m} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 2 | 3 | 44 | 365 | 395 |
| 6 | 7 | 8 | 46 | 398 | 432 |
| 8 | 12 | 13 | 48 | 434 | 471 |
| 10 | 19 | 21 | 50 | 470 | 510 |
| 12 | 26 | 29 | 52 | 509 | 551 |
| 14 | 36 | 39 | 54 | 550 | 595 |
| 16 | 48 | 52 | 56 | 590 | 640 |
| 18 | 60 | 65 | 58 | 634 | 686 |
| 20 | 74 | 81 | 60 | 679 | 736 |
| 22 | 91 | 99 | 62 | 725 | 785 |
| 24 | 108 | 117 | 64 | 773 | 837 |
| 26 | 127 | 138 | 66 | 821 | 889 |
| 28 | 149 | 161 | 68 | 871 | 944 |
| 30 | 170 | 185 | 70 | 924 | 1001 |
| 32 | 192 | 208 | 72 | 977 | 1058 |
| 34 | 218 | 237 | 74 | 1032 | 1118 |
| 36 | 245 | 265 | 76 | 1090 | 1180 |
| 38 | 271 | 294 | 78 | 1147 | 1243 |
| 40 | 302 | 328 | 80 | 1207 | 1308 |
| 42 | 334 | 361 |  |  |  |

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Table 3-t ADJUSTMENT TABLE

| Calculated $(n-1)$ | Revised <br> $t$ | Calculated (n-1) | Revised |
| :---: | :---: | :---: | :---: |
| 1 | 12.70 | 16 | 2.12 |
| 2 | 4.30 | 17 | 2.11 |
| 3 | 3.18 | 18 | 2.10 |
| 4 | 2.78 | 19 | 2.09 |
| 5 | 2.57 | 20 | 2.09 |
| 6 | 2.45 | 21 | 2.08 |
| 7 | 2.36 | 22 | 2.07 |
| 8 | 2.31 | 23 | 2.07 |
| 9 | 2.26 | 24 | 2.06 |
| 10 | 2.23 | 25 | 2.06 |
| 11 | 2.20 | 26 | 2.06 |
| 12 | 2.18 | 27 | 2.05 |
| 13 | 2.16 | 28 | 2.05 |
| 14 | 2.14 | 29 | 2.05 |
| 15 | 2.13 |  |  |

Table 4 - Samples Required
( $\mathrm{t}=2, \mathrm{~A}= \pm 5 \%$ )
Coefficient of Variation \%

| Total Loads/ Trees | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 13 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 22 |
| 200 | 13 | 13 | 13 | 13 | 13 | 13 | 15 | 17 | 19 | 21 | 24 |
| 300 | 13 | 13 | 13 | 13 | 13 | 13 | 15 | 17 | 19 | 22 | 25 |
| 400 | 13 | 13 | 13 | 13 | 13 | 13 | 15 | 17 | 20 | 23 | 26 |
| 500 | 13 | 13 | 13 | 13 | 13 | 14 | 15 | 17 | 20 | 23 | 26 |
| 600 | 13 | 13 | 13 | 13 | 13 | 14 | 15 | 17 | 20 | 23 | 26 |
| 700 | 13 | 13 | 13 | 13 | 13 | 14 | 15 | 17 | 20 | 23 | 26 |
| 800 | 13 | 13 | 13 | 13 | 13 | 14 | 15 | 18 | 20 | 23 | 26 |
| 900 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1000 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1100 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1200 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1300 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1400 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1500 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1600 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1700 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 26 |
| 1800 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 1900 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2000 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2100 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2200 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2300 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2400 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2500 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2600 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2700 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2800 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 2900 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3000 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3100 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3200 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3300 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3400 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3500 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3600 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3700 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3800 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 3900 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4000 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4100 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4200 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4300 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4400 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4500 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 23 | 27 |
| 4600 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 24 | 27 |
| 4700 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 24 | 27 |
| 4800 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 24 | 27 |
| 4900 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 24 | 27 |
| 5000 | 13 | 13 | 13 | 13 | 13 | 14 | 16 | 18 | 20 | 24 | 27 |

Note: Adjustments have been made to t and CV values when the numbers of samples are below 30 .

Table 4 (cont'd) - Samples Required
$(t=2, A= \pm 5 \%)$
Coefficient of Variation \%

| Total <br> Loads/ <br> Trees | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 24 | 26 | 27 | 29 | 32 | 34 | 37 | 39 | 41 | 44 | 46 |
| 200 | 27 | 30 | 31 | 34 | 38 | 41 | 45 | 48 | 52 | 56 | 59 |
| 300 | 28 | 30 | 32 | 36 | 40 | 44 | 48 | 53 | 57 | 62 | 66 |
| 400 | 29 | 30 | 33 | 37 | 41 | 46 | 50 | 55 | 60 | 65 | 70 |
| 500 | 29 | 30 | 34 | 38 | 42 | 47 | 52 | 57 | 62 | 67 | 72 |
| 600 | 30 | 30 | 34 | 38 | 43 | 48 | 53 | 58 | 63 | 69 | 74 |
| 700 | 30 | 30 | 34 | 39 | 43 | 48 | 53 | 59 | 64 | 70 | 76 |
| 800 | 30 | 30 | 34 | 39 | 44 | 49 | 54 | 59 | 65 | 71 | 77 |
| 900 | 30 | 30 | 35 | 39 | 44 | 49 | 54 | 60 | 65 | 71 | 77 |
| 1000 | 30 | 30 | 35 | 39 | 44 | 49 | 55 | 60 | 66 | 72 | 78 |
| 1100 | 30 | 30 | 35 | 39 | 44 | 50 | 55 | 60 | 66 | 72 | 79 |
| 1200 | 30 | 31 | 35 | 40 | 45 | 50 | 55 | 61 | 67 | 73 | 79 |
| 1300 | 30 | 31 | 35 | 40 | 45 | 50 | 55 | 61 | 67 | 73 | 79 |
| 1400 | 30 | 31 | 35 | 40 | 45 | 50 | 55 | 61 | 67 | 73 | 80 |
| 1500 | 30 | 31 | 35 | 40 | 45 | 50 | 56 | 61 | 67 | 74 | 80 |
| 1600 | 30 | 31 | 35 | 40 | 45 | 50 | 56 | 62 | 68 | 74 | 80 |
| 1700 | 30 | 31 | 35 | 40 | 45 | 50 | 56 | 62 | 68 | 74 | 81 |
| 1800 | 30 | 31 | 35 | 40 | 45 | 50 | 56 | 62 | 68 | 74 | 81 |
| 1900 | 30 | 31 | 35 | 40 | 45 | 50 | 56 | 62 | 68 | 74 | 81 |
| 2000 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 68 | 75 | 81 |
| 2100 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 68 | 75 | 81 |
| 2200 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 68 | 75 | 82 |
| 2300 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 68 | 75 | 82 |
| 2400 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 68 | 75 | 82 |
| 2500 | 30 | 31 | 35 | 40 | 45 | 51 | 56 | 62 | 69 | 75 | 82 |
| 2600 | 30 | 31 | 36 | 40 | 45 | 51 | 57 | 62 | 69 | 75 | 82 |
| 2700 | 30 | 31 | 36 | 40 | 45 | 51 | 57 | 63 | 69 | 75 | 82 |
| 2800 | 30 | 31 | 36 | 40 | 45 | 51 | 57 | 63 | 69 | 75 | 82 |
| 2900 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 75 | 82 |
| 3000 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 75 | 82 |
| 3100 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 82 |
| 3200 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 82 |
| 3300 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3400 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3500 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3600 | 30 | 31 | 36 | 40 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3700 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3800 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 3900 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4000 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4100 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4200 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4300 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4400 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4500 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4600 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 69 | 76 | 83 |
| 4700 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 70 | 76 | 83 |
| 4800 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 70 | 76 | 83 |
| 4900 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 |  | 76 | 83 |
| 5000 | 30 | 31 | 36 | 41 | 46 | 51 | 57 | 63 | 70 | 76 | 83 |

Note: Adjustments have been made to $t$ and CV values when the numbers of samples are below 30 .

Table 5 - Percent Samples Required

$$
(\mathrm{t}=2, \mathrm{~A}= \pm 5 \%)
$$

Coefficient of Variation \%

| Total <br> Loads/ <br> Trees | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.2 | 14.4 | 16.0 | 17.7 | 19.8 | 22.0 |
| 200 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 7.3 | 8.4 | 9.4 | 10.7 | 12.1 |
| 300 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 | 4.4 | 5.0 | 5.7 | 6.5 | 7.4 | 8.4 |
| 400 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.8 | 4.3 | 4.9 | 5.6 | 6.3 |
| 500 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 | 2.7 | 3.0 | 3.4 | 3.9 | 4.5 | 5.1 |
| 600 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.5 | 2.9 | 3.3 | 3.8 | 4.3 |
| 700 | 1.9 | 1.9 | 1.9 | 1.9 | 1.9 | 1.9 | 2.2 | 2.5 | 2.8 | 3.2 | 3.7 |
| 800 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.7 | 1.9 | 2.1 | 2.5 | 2.8 | 3.2 |
| 900 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.5 | 1.7 | 1.9 | 2.2 | 2.5 | 2.9 |
| 1000 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.5 | 1.7 | 2.0 | 2.3 | 2.6 |
| 1100 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.4 | 1.6 | 1.8 | 2.1 | 2.3 |
| 1200 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.3 | 1.4 | 1.6 | 1.9 | 2.1 |
| 1300 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.3 | 1.5 | 1.7 | 2.0 |
| 1400 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.1 | 1.2 | 1.4 | 1.6 | 1.8 |
| 1500 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 1.1 | 1.3 | 1.5 | 1.7 |
| 1600 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 1.1 | 1.2 | 1.4 | 1.6 |
| 1700 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 1.0 | 1.1 | 1.3 | 1.5 |
| 1800 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 | 1.4 |
| 1900 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 |
| 2000 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.6 | 0.7 | 0.8 | 1.0 | 1.1 | 1.3 |
| 2100 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 |
| 2200 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 |
| 2300 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 1.0 | 1.1 |
| 2400 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.1 |
| 2500 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 |
| 2600 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 | 0.7 | 0.9 | 1.0 |
| 2700 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 2800 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 2900 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 3000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.6 | 0.7 | 0.8 |
| 3100 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.6 | 0.7 | 0.8 |
| 3200 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 |
| 3300 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 |
| 3400 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.6 | 0.7 |
| 3500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.4 | 0.5 | 0.5 | 0.6 | 0.7 |
| 3600 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 |
| 3700 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 |
| 3800 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 |
| 3900 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.6 |
| 4000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 | 0.6 |
| 4100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 |
| 4200 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 |
| 4300 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 |
| 4400 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 |
| 4500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 |
| 4600 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 |
| 4700 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 |
| 4800 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 |
| 4900 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 |
| 5000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 |

Note: Adjustments have been made to t and CV values when the numbers of samples are below 30 .

## Table 5 (Cont'd) -Percent Samples Required

( $\mathrm{t}=2, \mathrm{~A}= \pm 5 \%$ )

Coefficient of Variation \%

| Total <br> Loads/ <br> Trees | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 24.5 | 26.7 | 29.2 | 30.0 | 31.6 | 34.1 | 36.6 | 39.0 | 41.4 | 43.6 | 45.8 |
| 200 | 13.6 | 15.0 | 15.2 | 17.0 | 18.8 | 20.6 | 22.4 | 24.2 | 26.1 | 27.9 | 29.7 |
| 300 | 9.3 | 10.0 | 10.7 | 12.0 | 13.3 | 14.7 | 16.1 | 17.6 | 19.0 | 20.5 | 22.0 |
| 400 | 7.2 | 7.5 | 8.2 | 9.3 | 10.3 | 11.5 | 12.6 | 13.8 | 15.0 | 16.2 | 17.5 |
| 500 | 5.8 | 5.9 | 6.7 | 7.5 | 8.4 | 9.4 | 10.4 | 11.3 | 12.4 | 13.4 | 14.5 |
| 600 | 4.9 | 4.9 | 5.6 | 6.3 | 7.1 | 7.9 | 8.8 | 9.6 | 10.5 | 11.4 | 12.4 |
| 700 | 4.2 | 4.2 | 4.8 | 5.5 | 6.2 | 6.9 | 7.6 | 8.4 | 9.2 | 10.0 | 10.8 |
| 800 | 3.7 | 3.7 | 4.3 | 4.8 | 5.4 | 6.1 | 6.7 | 7.4 | 8.1 | 8.8 | 9.6 |
| 900 | 3.3 | 3.3 | 3.8 | 4.3 | 4.8 | 5.4 | 6.0 | 6.6 | 7.3 | 7.9 | 8.6 |
| 1000 | 3.0 | 3.0 | 3.4 | 3.9 | 4.4 | 4.9 | 5.5 | 6.0 | 6.6 | 7.2 | 7.8 |
| 1100 | 2.7 | 2.7 | 3.1 | 3.5 | 4.0 | 4.5 | 5.0 | 5.5 | 6.0 | 6.6 | 7.1 |
| 1200 | 2.5 | 2.5 | 2.9 | 3.3 | 3.7 | 4.1 | 4.6 | 5.1 | 5.6 | 6.1 | 6.6 |
| 1300 | 2.3 | 2.3 | 2.6 | 3.0 | 3.4 | 3.8 | 4.3 | 4.7 | 5.1 | 5.6 | 6.1 |
| 1400 | 2.1 | 2.1 | 2.5 | 2.8 | 3.2 | 3.6 | 4.0 | 4.4 | 4.8 | 5.2 | 5.7 |
| 1500 | 2.0 | 2.0 | 2.3 | 2.6 | 2.9 | 3.3 | 3.7 | 4.1 | 4.5 | 4.9 | 5.3 |
| 1600 | 1.8 | 1.9 | 2.2 | 2.4 | 2.8 | 3.1 | 3.5 | 3.8 | 4.2 | 4.6 | 5.0 |
| 1700 | 1.7 | 1.8 | 2.0 | 2.3 | 2.6 | 3.0 | 3.3 | 3.6 | 4.0 | 4.4 | 4.7 |
| 1800 | 1.6 | 1.7 | 1.9 | 2.2 | 2.5 | 2.8 | 3.1 | 3.4 | 3.8 | 4.1 | 4.5 |
| 1900 | 1.5 | 1.6 | 1.8 | 2.1 | 2.3 | 2.7 | 3.0 | 3.3 | 3.6 | 3.9 | 4.3 |
| 2000 | 1.5 | 1.5 | 1.7 | 2.0 | 2.2 | 2.5 | 2.8 | 3.1 | 3.4 | 3.7 | 4.1 |
| 2100 | 1.4 | 1.4 | 1.6 | 1.9 | 2.1 | 2.4 | 2.7 | 3.0 | 3.3 | 3.6 | 3.9 |
| 2200 | 1.3 | 1.4 | 1.6 | 1.8 | 5.0 | 2.3 | 2.6 | 2.8 | 3.1 | 3.4 | 3.7 |
| 2300 | 1.3 | 1.3 | 1.5 | 1.7 | 1.9 | 2.2 | 2.4 | 2.7 | 3.0 | 3.3 | 3.5 |
| 2400 | 1.2 | 1.2 | 1.4 | 1.6 | 1.8 | 2.1 | 2.4 | 2.6 | 2.9 | 3.1 | 3.4 |
| 2500 | 1.2 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 | 2.3 | 2.5 | 2.7 | 3.0 | 3.3 |
| 2600 | 1.1 | 1.1 | 1.3 | 1.5 | 1.7 | 2.0 | 2.2 | 2.4 | 2.6 | 2.9 | 3.2 |
| 2700 | 1.1 | 1.1 | 1.3 | 1.4 | 1.6 | 1.9 | 2.1 | 2.3 | 2.5 | 2.8 | 3.0 |
| 2800 | 1.0 | 1.1 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.5 | 2.7 | 2.9 |
| 2900 | 1.0 | 1.0 | 1.2 | 1.3 | 1.5 | 1.8 | 2.0 | 2.2 | 2.4 | 2.6 | 2.8 |
| 3000 | 1.0 | 1.0 | 1.1 | 1.3 | 1.5 | 1.7 | 1.9 | 2.1 | 2.3 | 2.5 | 2.7 |
| 3100 | 0.9 | 1.0 | 1.1 | 1.3 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 | 2.7 |
| 3200 | 0.9 | 0.9 | 1.1 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 | 2.6 |
| 3300 | 0.9 | 0.9 | 1.0 | 1.2 | 1.3 | 1.5 | 1.7 | 1.9 | 2.1 | 2.3 | 2.5 |
| 3400 | 0.8 | 0.9 | 1.0 | 1.1 | 1.3 | 1.5 | 1.7 | 1.8 | 2.0 | 2.2 | 2.4 |
| 3500 | 0.8 | 0.8 | 1.0 | 1.1 | 1.3 | 1.5 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 |
| 3600 | 0.8 | 0.8 | 0.9 | 1.1 | 1.2 | 1.4 | 1.6 | 1.7 | 1.9 | 2.1 | 2.3 |
| 3700 | 0.8 | 0.8 | 0.9 | 1.0 | 1.2 | 1.4 | 1.5 | 1.7 | 1.9 | 2.1 | 2.2 |
| 3800 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 | 1.5 | 1.7 | 1.8 | 2.0 | 2.2 |
| 3900 | 0.7 | 0.7 | 0.9 | 1.0 | 1.1 | 1.3 | 1.5 | 1.6 | 1.8 | 1.9 | 2.1 |
| 4000 | 0.7 | 0.7 | 0.8 | 1.0 | 1.1 | 1.3 | 1.4 | 1.6 | 1.7 | 1.9 | 2.1 |
| 4100 | 0.7 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 | 1.4 | 1.5 | 1.7 | 1.9 | 2.0 |
| 4200 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.4 | 1.5 | 1.7 | 1.8 | 2.0 |
| 4300 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 | 1.5 | 1.6 | 1.8 | 1.9 |
| 4400 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 | 1.4 | 1.6 | 1.7 | 1.9 |
| 4500 | 0.6 | 0.6 | 0.7 | 0.9 | 1.0 | 1.1 | 1.3 | 1.4 | 1.5 | 1.7 | 1.8 |
| 4600 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 | 1.4 | 1.5 | 1.7 | 1.8 |
| 4700 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 | 1.3 | 1.5 | 1.6 | 1.8 |
| 4800 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.1 | 1.2 | 1.3 | 1.4 | 1.6 | 1.7 |
| 4900 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 | 1.4 | 1.6 | 1.7 |
| 5000 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.3 | 1.4 | 1.5 | 1.7 |

Note: Adjustments have been made to t and CV values when the numbers of samples are below 30 .

DEVELOPMENT

## Table 6 - Summary of General Conversion Factors

Conversion factors are generally average values.

## Volume

1 cubic metre $(\mathrm{m} 3)=35.315$ cubic feet
1 cord $=128$ cubic feet (air and bark)
1 cord $=85$ cubic feet (solid)

## Fuelwood

Solid means the actual roundwood volume whereas stacked represents the solid volume plus air and bark. Due to the fact that deciduous is less cylindrical and has more branching than coniferous, there is less solid volume for a given cord or stacked m3.

## Coniferous

$1 \operatorname{cord}($ solid $)=2.407 \mathrm{~m} 3$ (solid)
$1 \mathrm{~m} 3($ stacked $)=0.664 \mathrm{~m} 3($ solid $)$

## Deciduous

$1 \operatorname{cord}($ solid $)=2.010 \mathrm{~m} 3$ (solid)
$1 \mathrm{~m} 3($ stacked $)=0.557 \mathrm{~m} 3($ solid $)$

## Lumber

$1 \mathrm{~m} 3=233$ foot board measure (fbm)

## Wood Chips

$$
\begin{aligned}
1 \text { bone dry unit } & =1.089 \text { tonnes } \\
& =100 \mathrm{cubic} \text { feet } \\
& =2.603 \mathrm{~m} 3(\text { solid })
\end{aligned}
$$

Table 7 - Smalian Half Volume Table


